

# MOTION OF A THIN LAYER OF A HEAVY FLUID OVER THE SURFACE OF A SOLID BODY

(O DVIZHENII TONKOGO SLOIA TIAZHELOI ZHIDKOSTI  
PO POVERKHNOSTI TVERDOGO TELA)

PMM Vol.29, № 5, 1965, pp. 950-951

A.F.FROLOV  
(Moscow)

(Received March 30, 1965)

1. Potential flow of an ideal weightless fluid, spreading in a thin layer over the surface of a solid body, was considered in [1 and 2]. The equations of a plane flow of a slightly curved jet of a heavy fluid of the type considered here have the form [3]:

$$v_s \frac{\partial v_s}{\partial s} + v_r \frac{\partial v_s}{\partial r} = -\frac{1}{\rho} \frac{\partial p}{\partial s} - g \frac{dy}{ds}, \quad -k(s)v_s^2 = -\frac{1}{\rho} \frac{\partial p}{\partial r} + g \frac{dx}{ds}$$

$$\frac{\partial v_s}{\partial s} + \frac{\partial v_r}{\partial r} = 0 \tag{1.1}$$

Here  $v_s, v_r$  are the components of the velocity of the fluid, measured along the axes of an auxiliary curvilinear system of coordinates  $s, r$ , in which  $r$  lies along a normal to the surface of the solid body, and  $s$  is the length of the arc of the directrix  $L_1$  of the cylindrical surface of the solid body,  $p$  and  $\rho$  are, respectively, the pressure and the density of the fluid,  $g$  is the acceleration of gravity, directed against the  $y$ -axis of the basic orthogonal system of coordinates  $x = x(s)$  and  $y = y(s)$  are the equations of  $L_1$ , and  $k(s)$  is the curvature of  $L_1$ .

Transferring the origin of  $r$  to the free stream line  $L_0$ , we have for  $r = 0$

$$v_s = v_0(s), \quad v_r = 0, \quad p = p_0 = \text{const} \tag{1.2}$$

On the basis of the Bernoulli integral for a steady motion, we have  $v_0^2(s) = c_0 - 2gy(s)$ . We shall regard the thickness of the stream  $h(s)$ , measured along the normal to the surface of the solid body, as a small quantity of the first order.

In view of this, velocity  $v_s$  can be expressed in the form

$$v_s(s, r) = v_0(s) + u(s, r) \tag{1.3}$$

where  $u(s, r)$  is a quantity of the first order of magnitude. Substituting (1.3) into the second equation of system (1.1) and bearing in mind that  $k(s)$  is also a small quantity of the first order, we ignore the terms of the second and higher orders,

$$k(s)v_0^2(s) + g \frac{dx}{ds} = \frac{1}{\rho} \frac{\partial p}{\partial r}$$

From this, taking into account conditions (1.2), we obtain the pressure in the stream

$$p = \rho \left[ k(s) v_0^2(s) + g \frac{dx}{ds} \right] r + p_0 \quad (1.4)$$

Using this equation to eliminate pressure  $p$  in the first equation of system (1.1) and introducing the usual stream function  $\psi(s, r)$  defined by

$$v_s = \frac{\partial \psi}{\partial r}, \quad v_r = -\frac{\partial \psi}{\partial s}$$

we obtain the following nonlinear equation for the stress function

$$\frac{\partial \psi}{\partial r} \frac{\partial^2 \psi}{\partial r \partial s} - \frac{\partial \psi}{\partial s} \frac{\partial^2 \psi}{\partial r^2} + \frac{d}{ds} \left[ k(s) v_0^2(s) + g \frac{dx}{ds} \right] r + g \frac{dy}{ds} = 0 \quad (1.5)$$

By reference to (1.3), the stream function  $\psi(s, r)$  can be expressed in the form

$$\psi(s, r) = \psi_0(s, r) + \psi_1(s, r) \quad (1.6)$$

where  $\psi_0 = r v_0(s)$ , and function  $\psi_1(s, r)$  is one order of magnitude smaller than  $\psi_0(s, r)$ . Ignoring in Equation (1.5) all terms involving the products of derivatives of function  $\psi_1(s, r)$  we obtain the linear equation

$$v_0(s) \frac{\partial^2 \psi_1}{\partial r \partial s} + \frac{dv_0}{ds} \frac{\partial \psi_1}{\partial r} - r \frac{dv_0}{ds} \frac{\partial^2 \psi_1}{\partial r^2} + r \frac{d}{ds} \left[ k(s) v_0^2(s) + g \frac{dx}{ds} \right] = 0 \quad (1.7)$$

The solution of this equation, satisfying also the conditions of (1.2), is

$$\psi_1(s, r) = r^2 f(s), \quad \frac{df}{ds} = -\frac{1}{2v_0(s)} \frac{d}{ds} \left[ k(s) v_0^2(s) + g \frac{dx}{ds} \right] \quad (1.8)$$

Thus, the stream function of a slightly curved jet of a heavy fluid (to the present degree of accuracy) is

$$\psi(s, r) = r v_0(s) - r^2 \left( \frac{d}{ds} \left[ v_0^2(s) k(s) + g \frac{dx}{ds} \right] \frac{ds}{2v_0(s)} + c_1 \right) \quad (1.9)$$

To determine the constant  $c_1$  it is necessary to specify the velocities  $v_r$  and  $v_s$  and the pressure  $p$  at the initial section  $s = s_0$  in the form

$$v_r = \alpha r + \beta r^2, \quad v_s = v_0(s_0) + \delta r, \quad p = p_0 + \lambda r \quad (\alpha, \beta, \delta, \lambda - \text{const})$$

where  $\alpha, \beta, \lambda$  are explicitly defined in terms of the geometric characteristics of the surface over which the flow takes place at  $s = s_0$  and  $\delta = c_1$ . The thickness of the jet is determined from the condition  $\psi(s, h) = Q$ , where  $Q$  is the rate of flow, since  $L_1$  is the streamline.

2. We shall now use these relationships to determine the shape of the jet of a heavy fluid on the basis of the given distribution of pressure  $p_1$  along the streamline  $L_1$ . Determining the thickness of the jet  $h(s)$  to the first approximation [1] on the basis of the velocity  $v_0(s)$ , we obtain from (1.4) the following equation for the shape of the jet:

$$k(s) v_0^2(s) + g \frac{dx}{ds} = \frac{v_0(s) \Delta p}{Q} \quad (\Delta p = p_1 - p_0) \quad (2.1)$$

Let  $p_1$  be a known function  $p_1(y)$ , that is  $p_1 = p_1(y)$ . It is known [4] that

$$k(s) = \frac{d^2 y}{ds^2} \left[ 1 - \left( \frac{dy}{ds} \right)^2 \right]^{-1/2}, \quad dx^2 + dy^2 = ds^2 \quad (2.2)$$

Therefore, stipulating that  $dy/ds = P(y)$ , we obtain from (2.1)

$$-(c_0 - 2gy) \frac{d}{dy} \sqrt{1 - B^2} + g \sqrt{1 - B^2} = \frac{\Delta p(y)}{Q} \sqrt{c_0 - 2gy} \quad (2.3)$$

Whence,

$$1 - \left(\frac{dy}{ds}\right)^2 = \frac{J^2(y)}{c_0 - 2gy} \quad \left(J(y) = \int \frac{\Delta p(y)}{Q} dy + c_2\right) \quad (2.4)$$

Using (2.2) to eliminate the length of the arc, we shall obtain the following double quadrature which we can use to define the equation of the trajectory of the jet:

$$x = \int \frac{J(y) dy}{[c_0 - 2gy - J^2(y)]^{1/2}} + c_3 \quad (2.5)$$

The constants  $c_2$  and  $c_3$  are determined from the initial point  $y(x_0)$  and the initial slope  $y'(x_0)$  of the jet. Let us now consider some particular cases.

a) Let  $\Delta p = 0$ ,  $p_1 = p_0$ . The trajectory of the free falling jet will be a parabola

$$2gy = (c_0 - c_2^2) - \frac{4g^2(x - c_3)^2}{c_2^2}$$

b) In the case of impact of a jet of heavy fluid against the surface of a static heavy fluid with specific gravity  $\gamma$ , when at the interface of the jet and the static fluid there is a discontinuity in the velocities, and the pressure can be assumed equal to the hydrostatic pressure. The trajectory of the jet will be defined by the quadrature

$$x = \int \frac{(1/2 \gamma Q^{-1} y^2 + c_2) dy}{[c_0 - 2gy - (1/2 \gamma Q^{-1} y^2 + c_2)^2]^{1/2}} + c_3 \quad (2.6)$$

#### BIBLIOGRAPHY

1. Frankl', F.I., Priblizhennyi raschet struinogo potentsial'nogo techenia zhidkosti, rasprostraniayushchegosia po poverkhnosti tverdogo tela tonkim sloem (Approximate calculation of the potential flow of a jet of fluid flowing in a thin layer over the surface of a solid body). *PMM* Vol.24, № 2, 1960.
2. Volterra, V., Sur les jets liquides. *J.Math.pures appl.* 9 S., t.11, №1, 1932.
3. Frolov, A.P., Ploskaia slaboskrivlennaya struia ideal'noi neshhimaemoi zhidkosti (A plane slightly curved jet of a perfect incompressible fluid). *PMM* Vol.28, № 3, 1964.
4. Rashevskii, P.K., Kurs differentsial'noi geometrii (Course in Differential Geometry). Gostekhizdat, 1950.

Translated by S.K.